

Appendix: Critical Fracture Stress of a Plate with an Inclined Crack

Consider a large thick plate of steel contains a crack of length $2a = 5 \text{ mm}$ oriented at an angle $\beta = 30^\circ$ with respect to the direction of applied uniaxial stress σ (Figure 27). Assuming $K_{Ic} = 60 \text{ MPa}\sqrt{\text{m}}$, $E = 210 \text{ GPa}$, $\nu = 0.3$, here we calculate the angle of initial crack extension and the value of the critical stress σ_c for crack growth according to the strain energy density criterion when the stress σ is (a) tensile and (b) compressive.

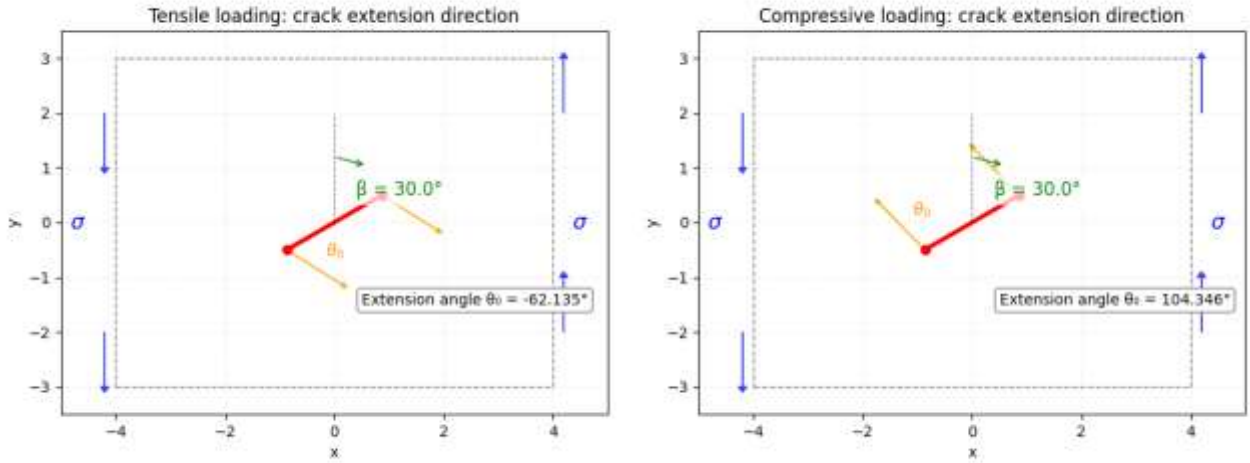


Figure 27. Geometry of an inclined centre crack in an infinite plate under uniaxial tensile stress.

The angle θ_0 of initial crack extension is calculated according to the strain energy density criterion by the relations :

$$\frac{\partial S}{\partial \theta} = 0, \quad \frac{\partial^2 S}{\partial \theta^2} > 0,$$

where S is the strain energy density factor and (r, θ) are polar coordinates measured from the crack tip.

S is given by:

$$S = a_{11}k_I^2 + 2a_{12}k_Ik_{II} + a_{22}k_{II}^2,$$

where the coefficients a_{ij} ($i, j = 1, 2$) are:

$$\begin{aligned} 16\mu a_{11} &= (1 + \cos\theta)(\kappa - \cos\theta), \\ 16\mu a_{12} &= \sin\theta[2\cos\theta - (\kappa - 1)], \\ 16\mu a_{22} &= (\kappa + 1)(1 - \cos\theta) + (1 + \cos\theta)(3\cos\theta - 1). \end{aligned}$$

In these equations, μ is the shear modulus, $k_i = K_i/\sqrt{\pi}$ ($i = I, II$), where K_I and K_{II} are the mode-I and mode-II stress intensity factors, and $\kappa = 3 - 4\nu$ for plane strain, or $\kappa = (3 - \nu)/(1 + \nu)$ for plane stress.

Crack initiation occurs when:

$$S_{\min} = S_c,$$

where S_c is the critical value of the strain energy density factor, a material constant given by:

$$S_c = \frac{(1 + \nu)(1 - 2\nu)K_{Ic}^2}{2\pi E}.$$

Consider a central crack of length $2a$ in an infinite plate subjected to a uniform uniaxial stress σ at infinity; suppose the axis of the crack makes an angle β with the direction of stress σ . The stress intensity factors are:

$$K_I = \sigma\sqrt{\pi a}\sin^2\beta, \quad K_{II} = \sigma\sqrt{\pi a}\sin\beta\cos\beta.$$

The crack extension angle θ_c is obtained from:

$$(\kappa - 1)\sin(\theta_c - 2\beta) - 2\sin[2(\theta_c - \beta)] - \sin 2\theta_c = 0, \quad \beta \neq 0.$$

For a thick plate, plane strain conditions dominate: $\kappa = 3 - 4\nu = 3 - 4(0.3) = 1.8$. With $\beta = 30^\circ$, Equation (9) becomes:

$$0.8\sin(\theta_c - 60^\circ) - 2\sin[2(\theta_c - 30^\circ)] - \sin 2\theta_c = 0.$$

The first root of this equation corresponding to tensile applied stress σ which satisfies $\partial^2 S / \partial \theta^2 > 0$ is:

$$\boxed{\theta_c = -62.135^\circ}.$$

This root yields:

$$\frac{1}{\sigma^2} \frac{\partial^2 S}{\partial \theta^2} = 4.69 > 0.$$

The critical value S_c is:

$$S_c = \frac{(1 + 0.3)(1 - 0.6)(60)^2}{2\pi(210 \times 10^3)} = 1.42 \times 10^{-3} \text{ MPa} \cdot \text{m}.$$

The shear modulus μ is:

$$\mu = \frac{E}{2(1+\nu)} = \frac{210}{2(1.3)} = 80.77 \text{ GPa.}$$

The coefficients a_{ij} at $\theta_c = -62.135^\circ$ are:

$$\begin{aligned} 16\mu a_{11} &= 1.51314 \times 10^{-6} \text{ MPa}^{-1}, \\ 16\mu a_{12} &= -0.0922 \times 10^{-6} \text{ MPa}^{-1}, \\ 16\mu a_{22} &= 1.61063 \times 10^{-6} \text{ MPa}^{-1}. \end{aligned}$$

The strain energy density factor is:

$$\begin{aligned} S(\theta_c) &= \frac{\sigma^2(2.5 \times 10^{-3})}{16(80.77 \times 10^3)} [1.51314 \sin^2 30^\circ \\ &\quad + 2(-0.0922) \sin 30^\circ \cos 30^\circ + 1.61063 \cos^2 30^\circ] \\ &= 0.9415 \times 10^{-9} \sigma^2 \text{ MPa}^{-1} \text{m.} \end{aligned}$$

Setting $S(\theta_c) = S_c$ gives:

$$0.9415 \times 10^{-9} \sigma_c^2 = 1.42 \times 10^{-3},$$

$$\boxed{\sigma_c = 1228 \text{ MPa}}.$$

The initial crack extension angle is $\theta_c = -62.135^\circ$.

The second root of Equation (10) corresponding to compressive stress σ is:

$$\boxed{\theta_c = 104.346^\circ}.$$

The second derivative condition gives:

$$\frac{1}{\sigma^2} \frac{\partial^2 S}{\partial \theta^2} = 5.744 > 0.$$

The coefficients a_{ij} at $\theta_c = 104.346^\circ$ are:

$$\begin{aligned} 16\mu a_{11} &= 1.5404, \\ 16\mu a_{12} &= -1.255, \\ 16\mu a_{22} &= 2.1824. \end{aligned}$$

Then:

$$S(\theta_c) = 0.4522 \times 10^{-9} \sigma_c^2,$$

and setting $S(\theta_c) = S_c$ yields:

$$\sigma_c = 1772 \text{ MPa}.$$

The initial crack extension angle is $\theta_c = 104.346^\circ$. The resulting initial crack extension angles are $\theta_c = -62.135^\circ$ under tension and $\theta_c = 104.346^\circ$ under compression, as illustrated in Figure 28.

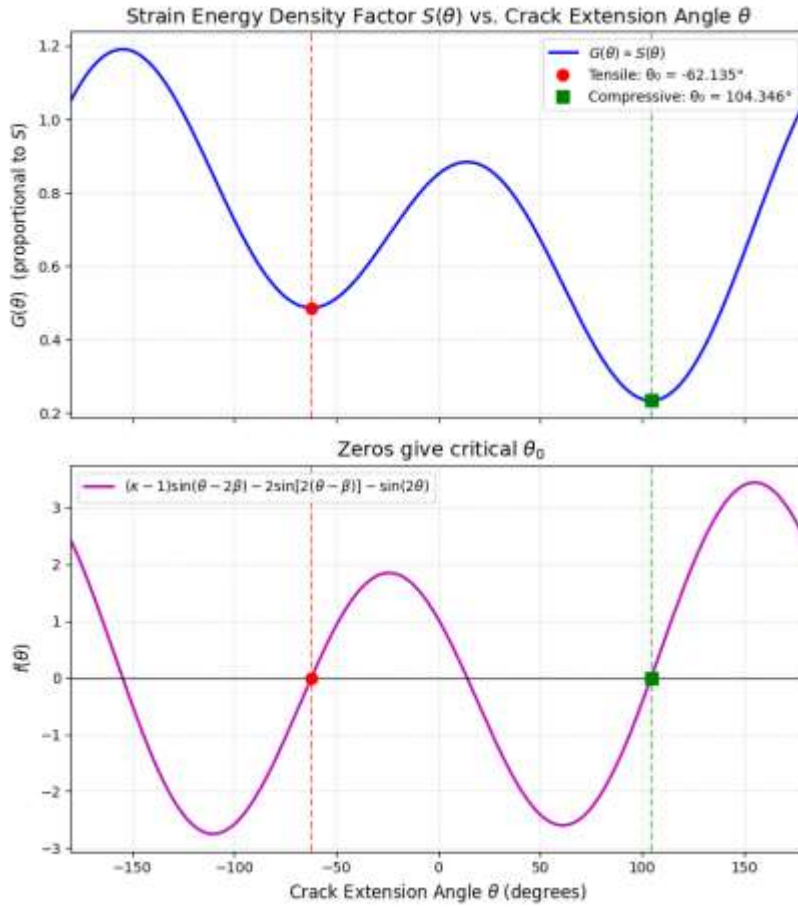


Figure 28. Predicted initial crack extension angles for tensile and compressive loading according to the strain energy density criterion.